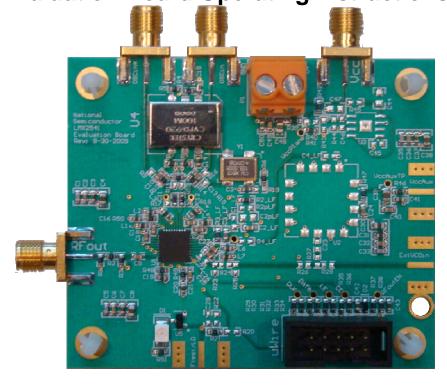


LMX2541 Family

Ultra Low Noise Frequency Synthesizer with Integrated VCO Evaluation Board Operating Instructions

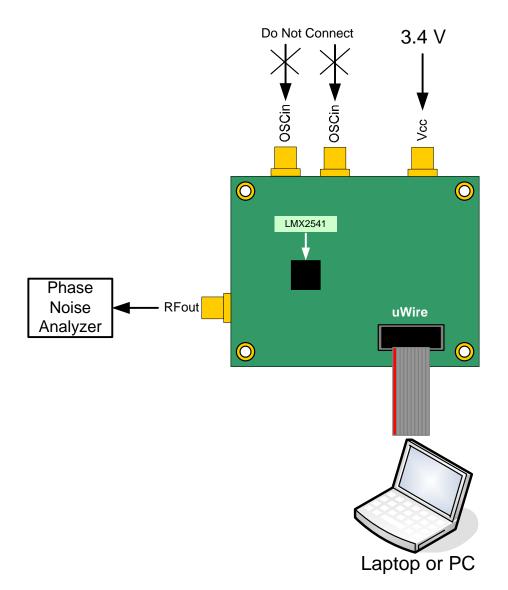


National Semiconductor Corporation High Speed Signal Path Division Precision Timing Devices 12-4-2009

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QUICK SETUP



<u>RFout</u>

Connect to a spectrum analyzer or phase noise analyzer. The Agilent E5052A was used for these instructions.

<u>Vcc</u>

Connect to a 3.4 volt low noise power supply

<u>uWire</u> Connect to a computer with CodeLoader software

ExtVCOin

This is not used in the default setup, but is included to support the use of an external VCO. In Full Chip Mode, this device has an on-chip VCO.

Ftest/LD

The LED is to ensure that the part is locked. This output can be very useful for diagnostic purposes

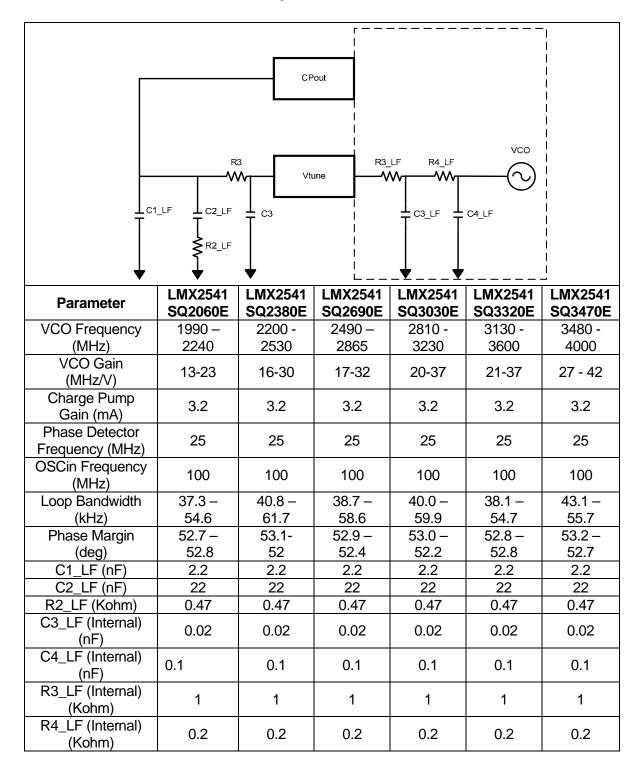
OSCin/OSCin*

This is not used in the default setup, but is included to support the use of an external OSCin signal. The board includes a 100 MHz TCXO, which has two varieties. The OSCin signal is absolutely critical for the phase noise and spur performance of the LMX2541.

Manufacturer	Model	Frequency	Comments		
Connor Winfield	CWX-813	100 MHz	Good phase noiseLow CostDrifts a lot.		
Crystek	CVPD920	100 MHz	Good Phase NoiseDrifts much lessHigh Cost		
National Semiconductor	LMK01000 LMK02000 LMK03000 LMK04000	Any	Eliminate drift issuesPotentially the best phase noiseBest for fractional spurs		

Be very aware of the TCXO drift and the contribution that it can have to phase noise. Termination of the TCXO has a large impact on fractional spurs as well. The best results can be achieved by driving this board with an LMK01000 LVPECL output. Doing so results in about a 4 dB spur improvement.

Loop Filter Values



* Note that the VCO gain does change a fair amount. Although not demonstrated in these instructions, the charge pump gain could be adjusted to account for this variation.

CodeLoader Setup Select the part. In this case, it is the LMX2541SQ3320E.

KLMX2541SQ3320	Ξ				
File Keyboard Controls	Select Device Options M	lode LPT/USB Help			
Port Setup	VCO PLL - Single Integer PLL - Dual Integer	Bits/Pins	BurstMode	PLL	
General	PLL - Fractional PLL + VCO Transceiver Clock Conditioners	LMX25415Q2060E LMX25415Q2380E LMX25415Q2690E	.oop Filter	− Program Pins	
MODE Full Chip MUX	3rd Order Modu DITH Weak	LMX25415Q3030E LMX25415Q3320E LMX25415Q3740E LMX2531LQ1146E	ms 💌	F EN_RFout*	

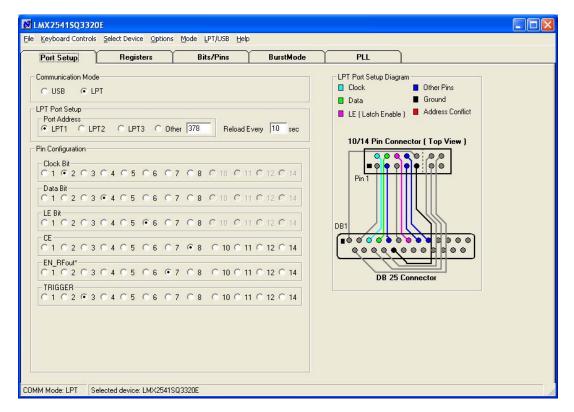
Choose the correct startup mode. This is determined by the part option.

M LMX2541SQ3320E	
File Keyboard Controls Select Device Options Mode LPT/USB Help	
Port Setup Registers Add Add Part Setup Add	
Show Bits Oscillator Doubler R Counter OSCin X1 4 Phase Charge Charge 100 MHz Phase Detector Pump Pump 100 MHz Frequency Plainty Gain State	

Load the part. You can load it from the menu or also press Cntrl + L.

	X2541SQ3320E					
File k	eyboard Controls Select De	vice Options I	Mode LPT/USB Help			
	Load Device Step Frequency	Ctrl+L	Bits/Pins	BurstMode		
Reo	Set VCO Frequency Set Comparison Frequency Set Crystal Frequency Reset Port	Ctrl+X	Counter Phase Detector	Phase Charge Detector Pump Polarity Gain	Charge Pump State	

On the Port Setup tab, the user may select the type of communication port (USB or Parallel) that will be used to program the device on the evaluation board. If parallel port is selected, the user should ensure that the correct port address is entered.

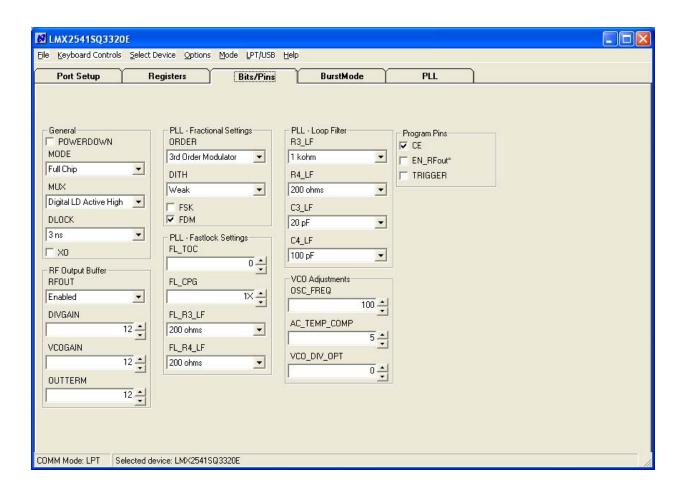


The Pin Configuration field is hardware dependent and normally <u>SHOULD NOT</u> be changed by the user.

The evaluation board is typically shipped with a parallel port cable that is used to interconnect the board to a PC LPT port, enabling the board to be programmed.

Separately available is a USB2UWIRE-IFACE board which simplifies evaluation by enabling the user to establish a USB connection from the Codeloader 4 software to the evaluation board. http://www.national.com/store/view_item/index.html?nsid=USB2UWIRE-IFACE

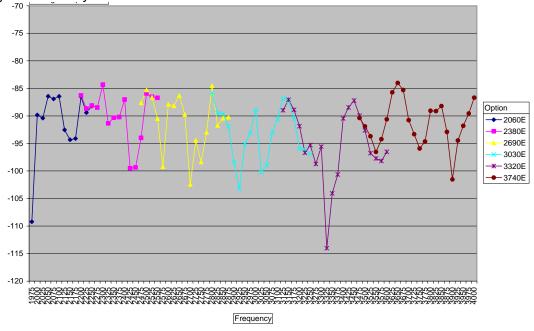
To view the function of any bit on the CodeLoader configuration tabs, place the cursor over the desired bit register label and click the right mouse button on it for a description. This Bits/Pins configuration is common to all options of the LMX2541 evaluation board.



Spurs

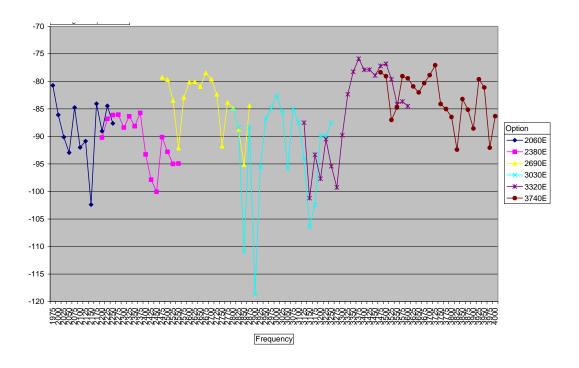
Oscillator Spurs

Oscillator spurs occur at the oscillator frequency (100 MHz) offset from the carrier. They can be largely impacted by the board layout. These were taken in 25 MHz increments.



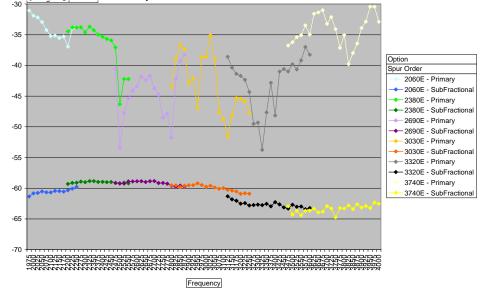
Reference (Phase Detector) Spurs

Reference spurs occur at a multiple of the phase detector frequency (25 MHz) from the carrier

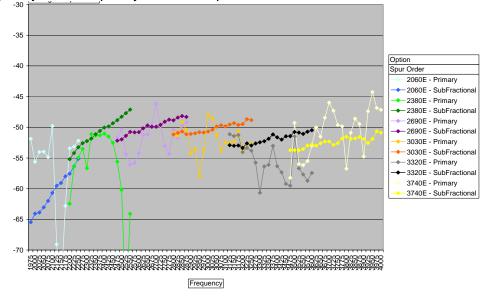


Fractional Spurs

In-band spurs occur inside the loop bandwidth. These spurs were measured with a WORST CASE fraction of 1/5000. The primary fractional spurs are at 5 kHz and the sub-fractional spurs are at 2.5 kHz. The actual frequency is the frequency in the chart plus 5 kHz.



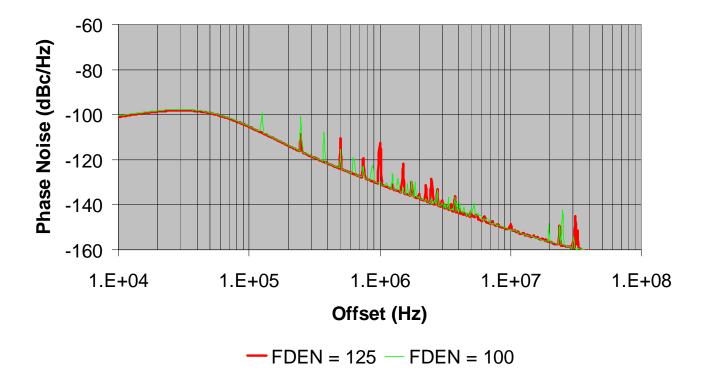
Out-band spurs occur inside the loop bandwidth. These spurs were measured with a WORST CASE fraction of 1/100. The primary fractional spurs are at 250 kHz and the sub-fractional spurs are at 125 kHz. The actual frequency is the frequency in the chart plus 250 kHz.

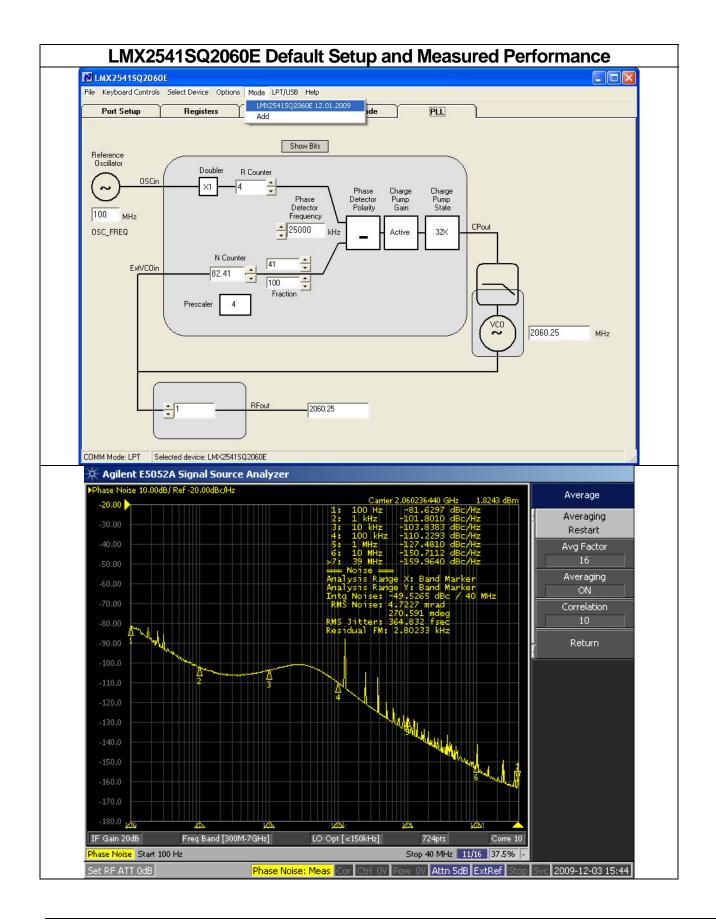


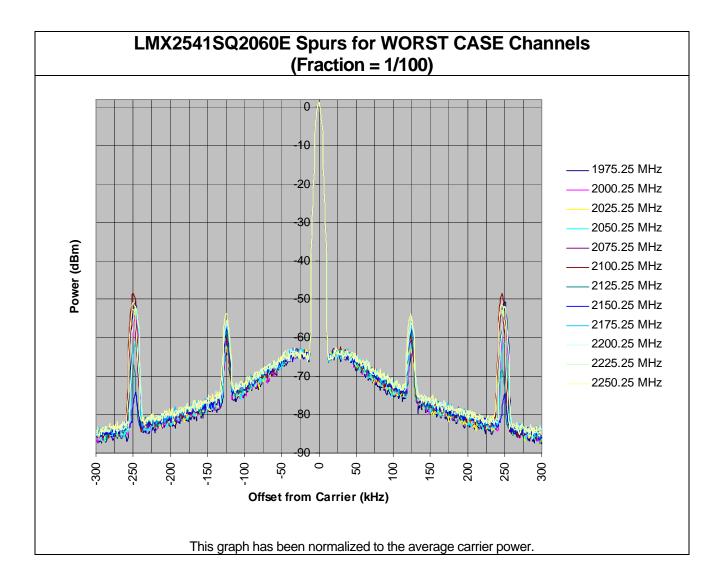
Minimizing Fractional Spurs

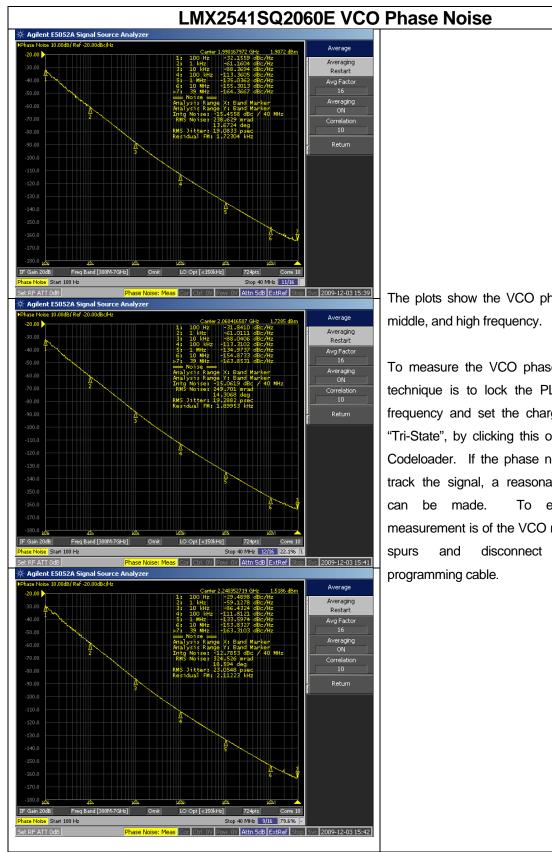
- Both fractional and sub-fractional spurs are highly sensitive to the OSCin signal. Higher slew rates are desired. Also, the termination makes a big difference. For this evaluation board, a series 120 ohm resistor had a large impact.
- The best results have been achieved when driving the part differentially with an LVPECL output of the LMK01000/2000/3000/400 series of clock conditioner devices from National Semiconductor.
- The spurs on this evaluation board are relatively high because the loop bandwidth is very wide. This wide loop bandwidth takes advantage of the close-in phase noise, but it does expose the fractional spurs more. The fractional spurs can be reduced by orders of magnitude by reducing the loop bandwidth. This requires a re-design of the loop filter.
- To eliminate the SubFractional spurs entirely, choose a fractional denominator with no factors of 2 or 3. For this 100 MHz TCXO and 250 kHz channel spacing, a phase detector frequency of 6.25 MHz and a fractional denominator of 25 would work. However, the higher N value does degrade the phase noise. An ideal scenario would be to use a TCXO frequency of something like 125 MHz. Then the sub-fractional spurs are eliminated if the phase detector is chosen to be 30.25 MHz and the fractional denominator is chosen to be 125.

In the plot below, one was taken with the default 100 MHz TCXO and another was taken with a 125 MHz signal. The phase detector frequency was changed to 31.25 MHz, but the charge pump gain was reduced to 26X to compensate for this. This is the same part, board, and frequency (3030.25 MHz). Although the fraction is different, notice that the fractional denominator of 125 has no sub fractional spurs at 125 kHz, 375 kHz, and so on. An LMK01000 evaluation board driven by a 1250 MHz signal was used to produce this 125 MHz signal.



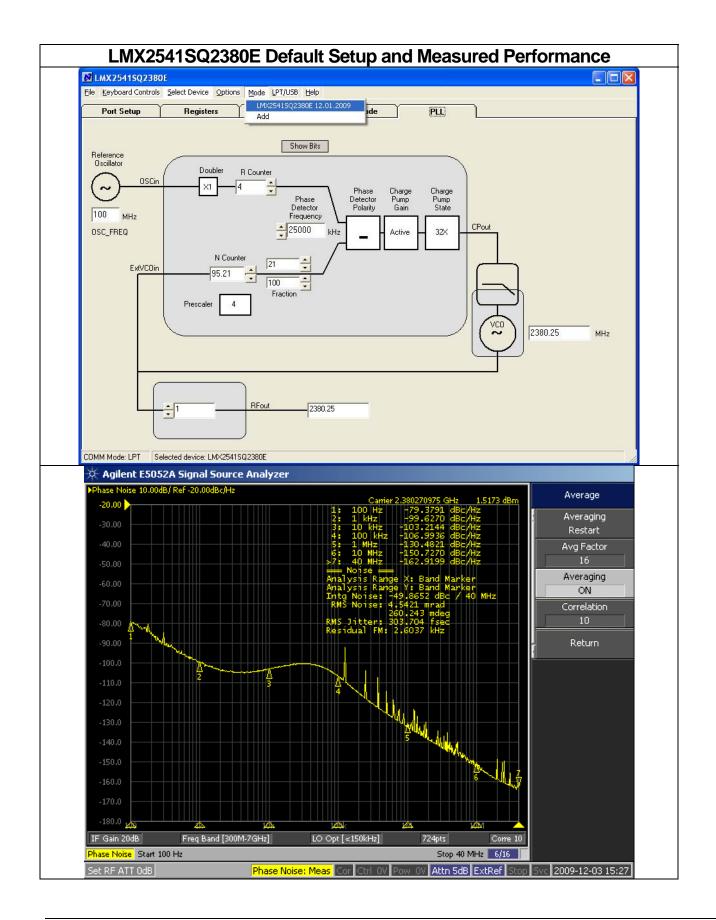


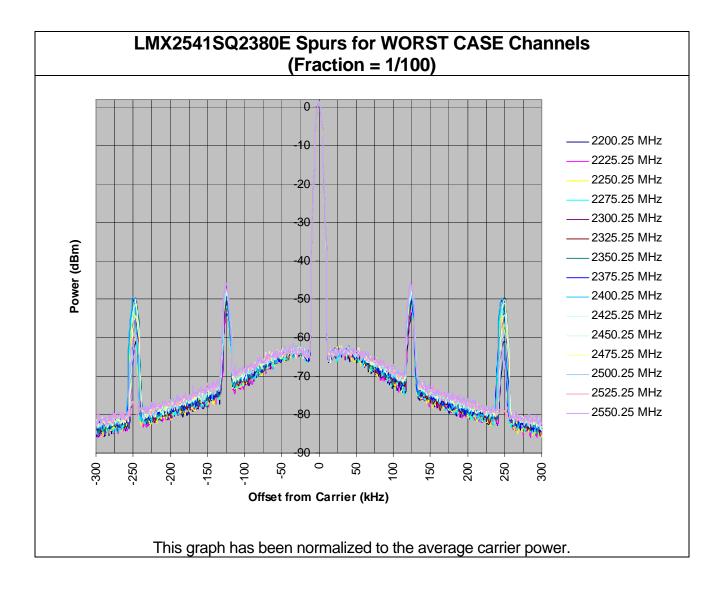


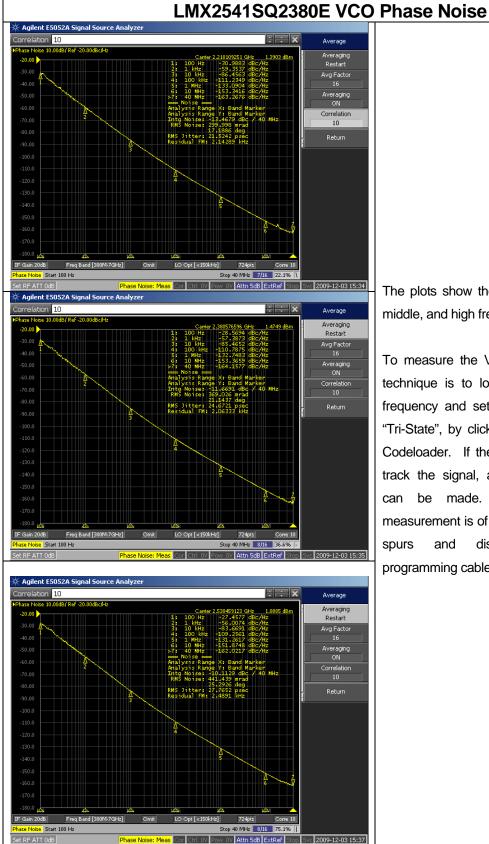


The plots show the VCO phase noise at low,

To measure the VCO phase noise, a simple technique is to lock the PLL to the desired frequency and set the charge pump state to "Tri-State", by clicking this on the PLL tab on Codeloader. If the phase noise analyzer can track the signal, a reasonable measurement To ensure that this measurement is of the VCO noise, omit the the the microwire



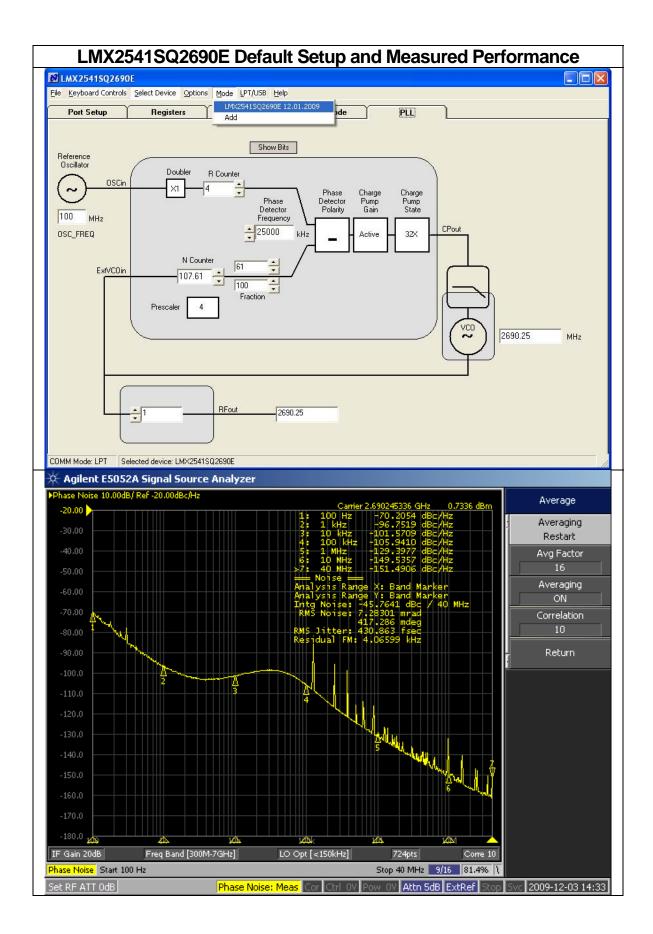


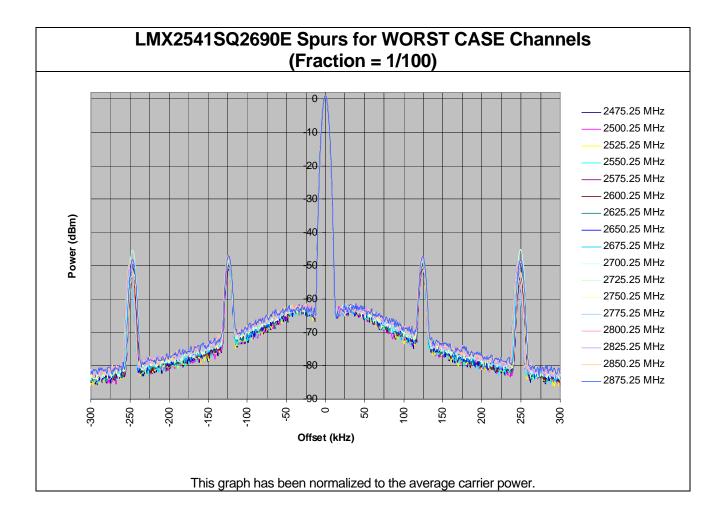


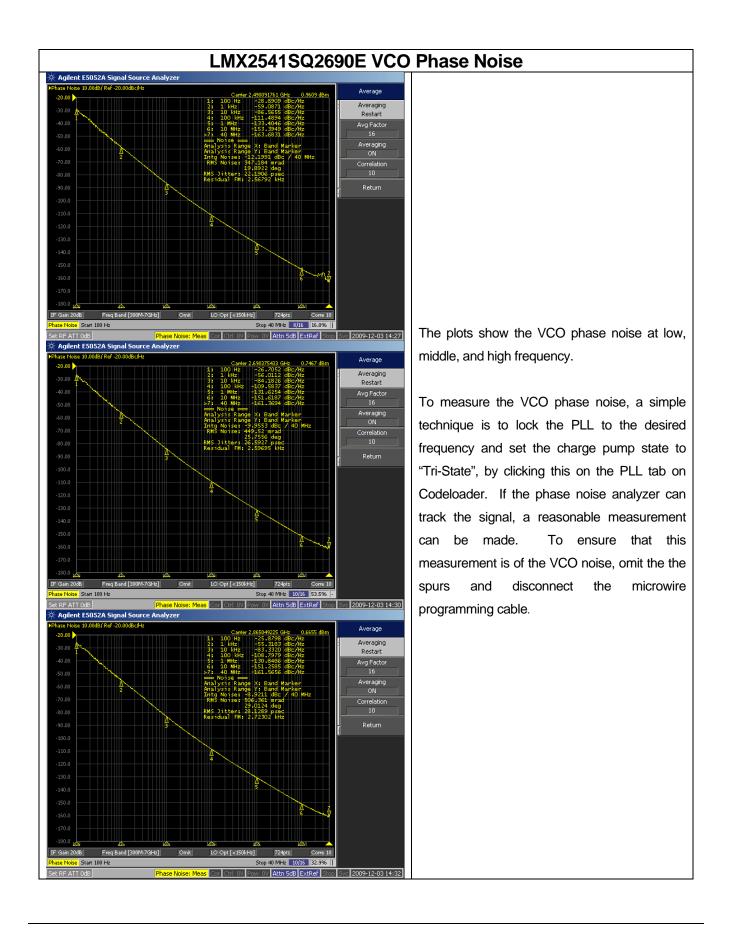
The plots show the VCO phase noise at low,

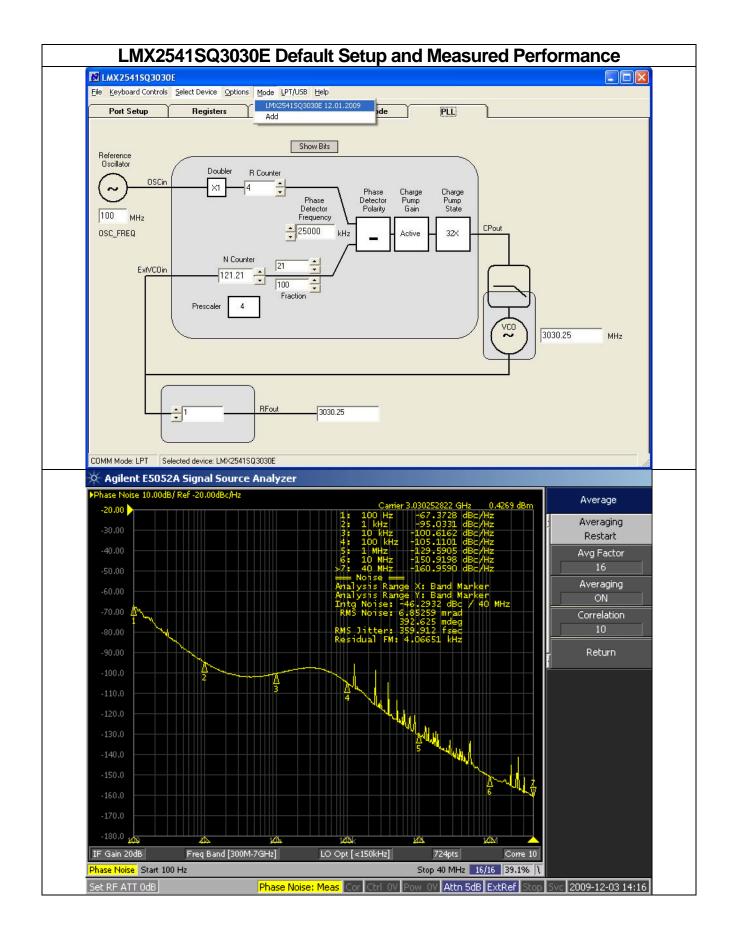
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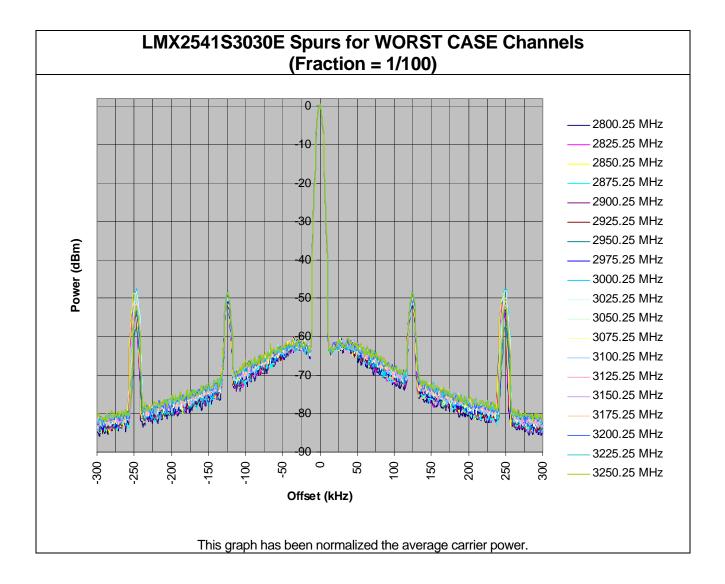
middle, and high frequency.

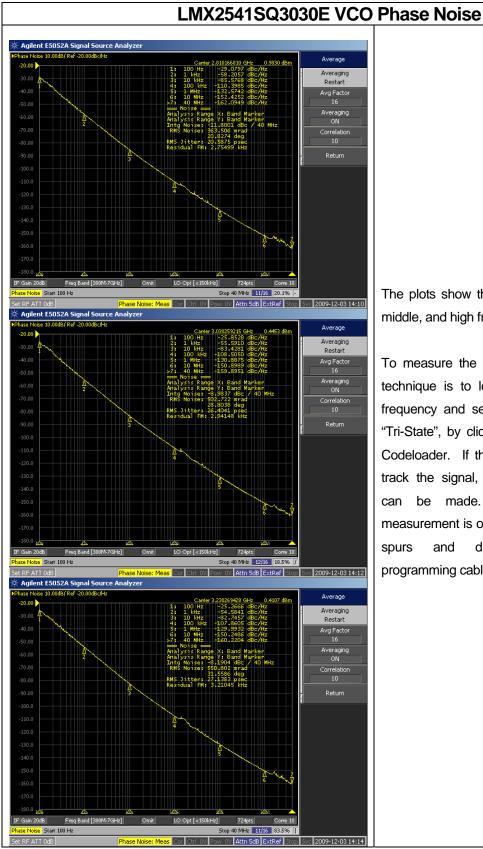






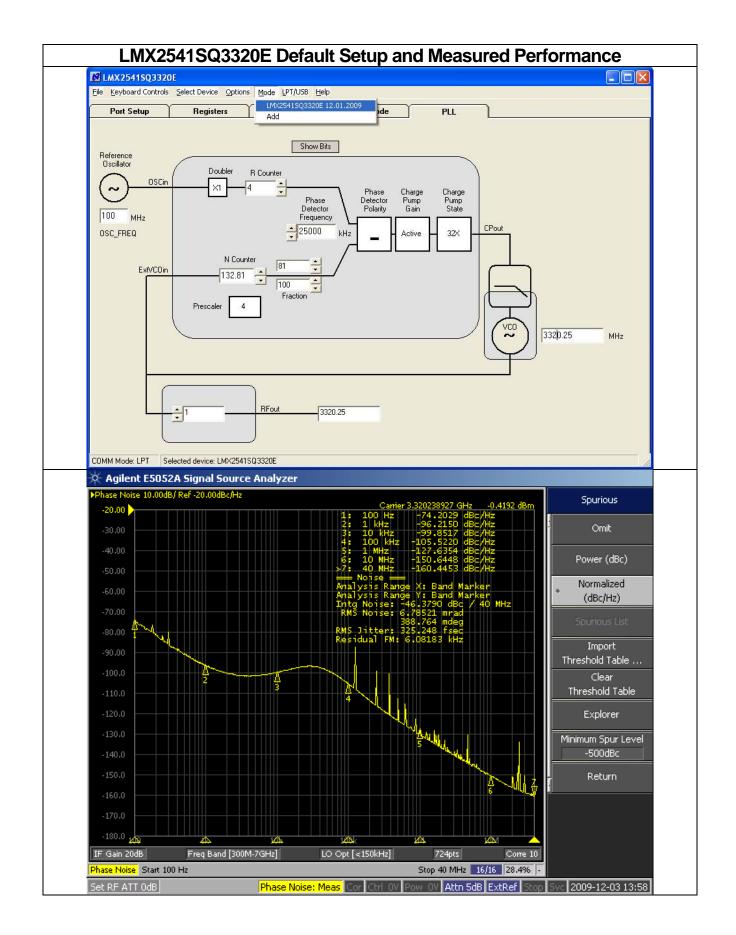


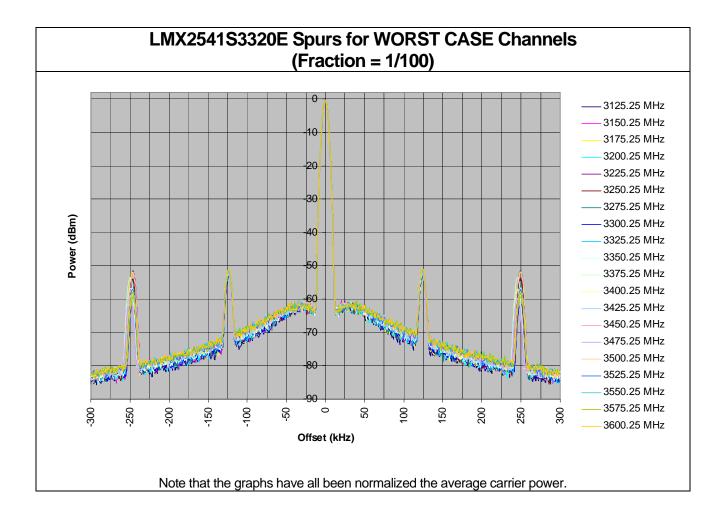


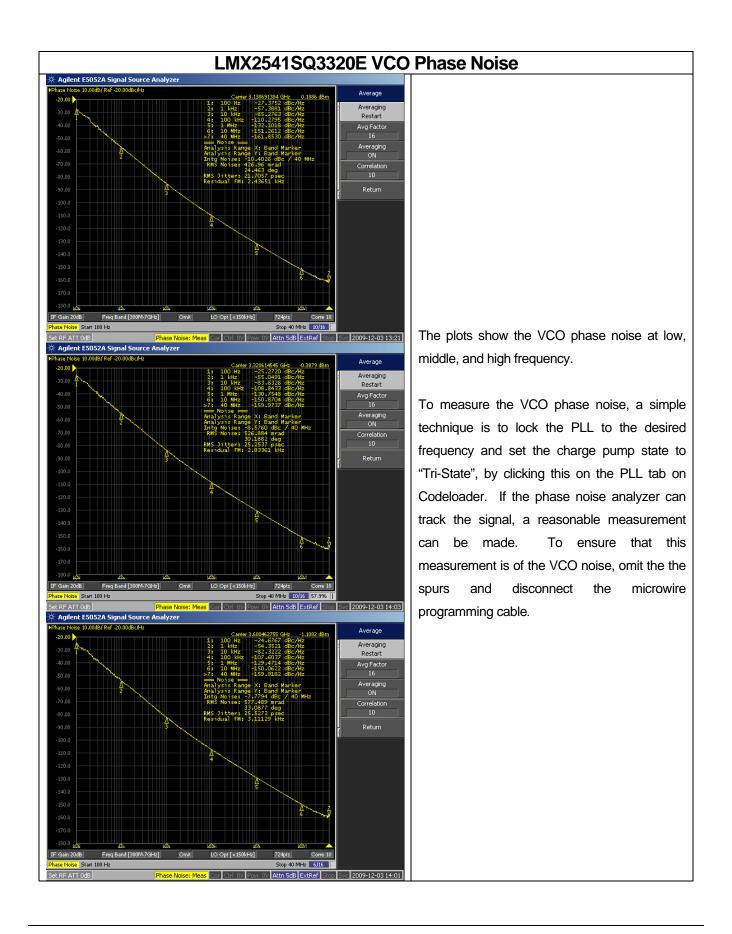


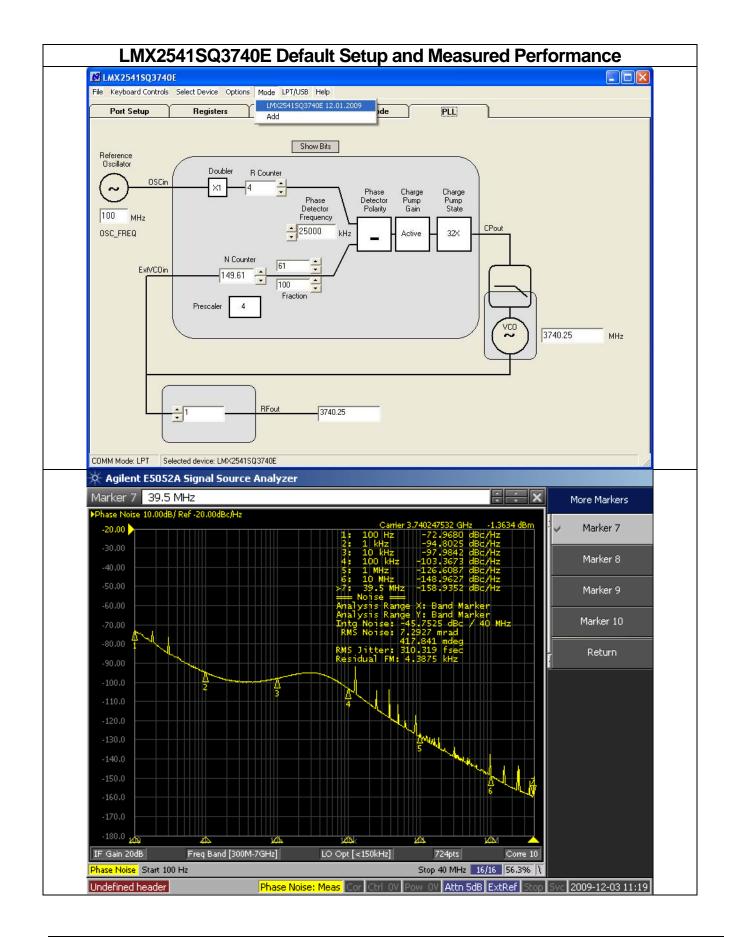
The plots show the VCO phase noise at low, middle, and high frequency.

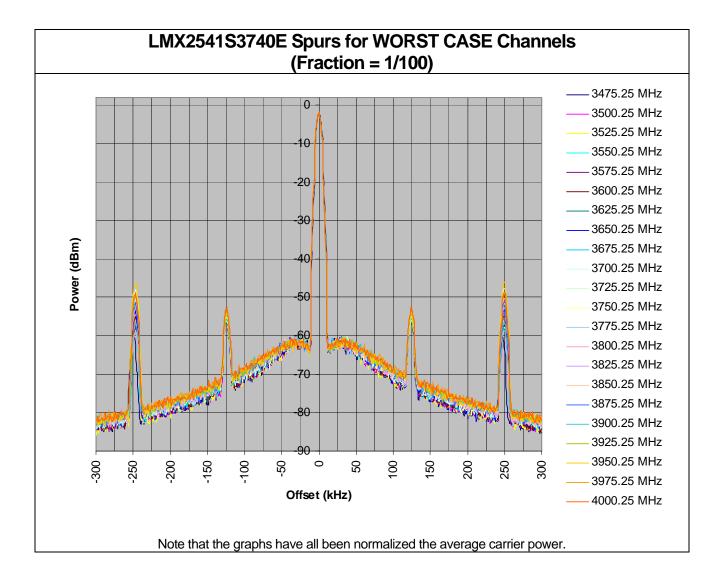
To measure the VCO phase noise, a simple technique is to lock the PLL to the desired frequency and set the charge pump state to "Tri-State", by clicking this on the PLL tab on Codeloader. If the phase noise analyzer can track the signal, a reasonable measurement can be made. To ensure that this measurement is of the VCO noise, omit the the spurs and disconnect the microwire programming cable.

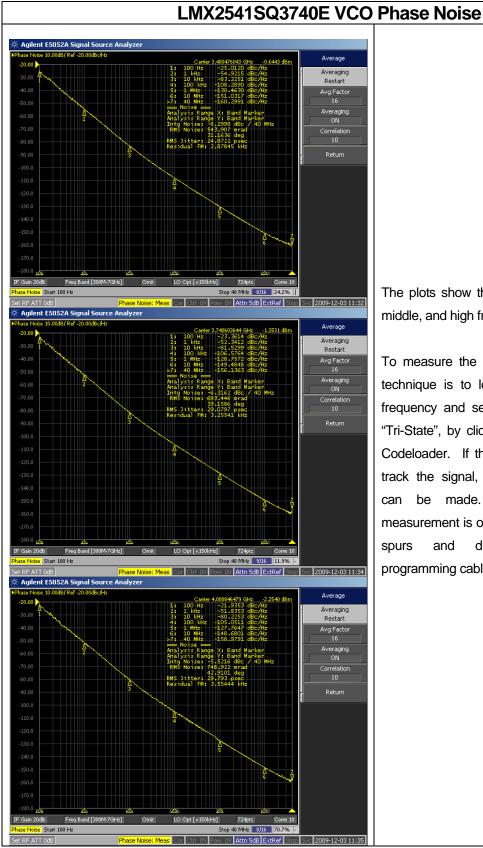










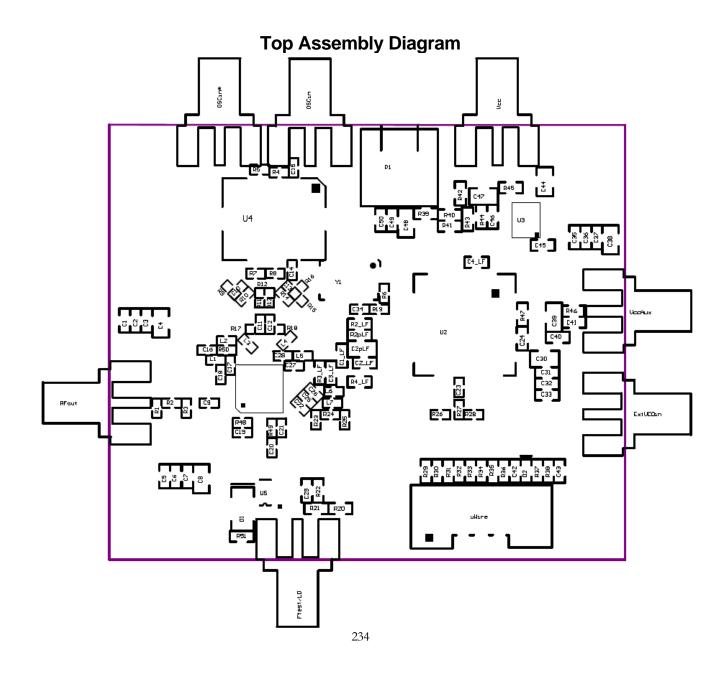


The plots show the VCO phase noise at low, middle, and high frequency.

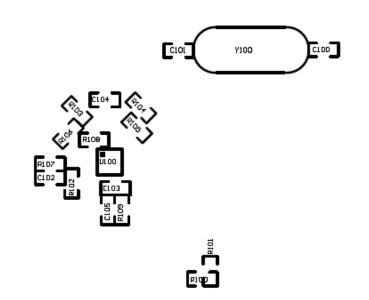
To measure the VCO phase noise, a simple technique is to lock the PLL to the desired frequency and set the charge pump state to "Tri-State", by clicking this on the PLL tab on Codeloader. If the phase noise analyzer can track the signal, a reasonable measurement can be made. To ensure that this measurement is of the VCO noise, omit the the spurs and disconnect the microwire programming cable.

Bill of Materials

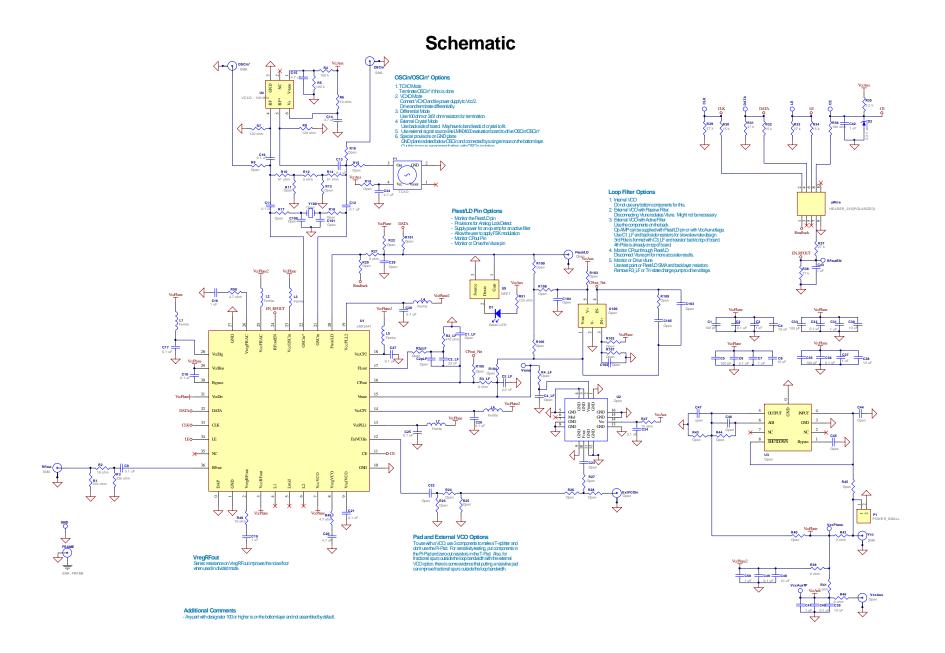
Revision	9/30/2009	Bill of	Malei	
Part	Manufacturer	Part Number	Qty	Identifier
T dit	Manufacturer		acitors	identifier
100 pF	Kemet	C0603C101J5GAC	4	C1, C5, C33, C35
2.2 nF	Kemet		4	
		C0603C222J5GAC		C3_LF
22 nF	Kemet	C0603C223K5RAC	1	C2_LF
0.1 uF	Kemet	C0603C104K5RAC	19	C2, C6, C9, C10, C11, C12, C13, C17, C18, C21, C24, C25, C26, C27, C28, C32, C36, C40, C49
1 uF	Kemet	C0603C105K8VAC	10	C3, C7, C16, C19, C31, C37, C41, C42, C43, C50
4.7 uF	Kemet	C0603C475K9PAC	4	C14, C15, C20, C34
10 uF	Kemet	C0805C106K9PAC	6	C4, C8, C30, C38, C39, C48
		Res	sistors	
0 ohm	Vishay/Dale	CRCW06030000Z0EA	7	R3_LF, R12, R21, R39, R41, R42, R46
4.7 ohm	Vishay/Dale	CRCW06034R7JNEA	2	R49, R50
10 ohm	Vishay/Dale	CRCW060310R0JNEA	3	R6, R47, R48
18 ohm	Vishay/Dale	CRCW060318R0JNEA	1	R2
51 ohm	Vishay/Dale	CRCW060351R0JNEA	2	R10, R14
120 ohm	Vishay/Dale	CRCW0603120RJNEA	3	R7, R8, R51
180 ohm	Vishay/Dale	CRCW0603180RJNEA	1	R36
	,		2	
330 ohm	Vishay/Dale	CRCW0603330RJNEA		R1, R3
470 ohm	Vishay/Dale	CRCW0603470RJNEA	1	R2_LF
2.2 k	Vishay/Dale	CRCW06032K20JNEA	1	R35
15 k	Vishay/Dale	CRCW060315K0JNEA	3	R30, R32, R34
27 k	Vishay/Dale	CRCW060327K0JNEA	5	R29, R31, R33, R37, R38
100 k	Vishay/Dale	CRCW0603100KJNEA	2	R4, R5
		C	ther	
Ferrite	Digikey	490-1015-1-ND	7	L1, L2, L3, L4, L5, L6, L7
3.3 V zener	Comchip	CZRU52C3V3	1	D2
HEADER_2X5 (POLARIZED)	FCI Electronics	52601-S10-8	1	uWire
Green LED	Lumex	SML-LX2832GC-TR	1	D1
POWER_SMALL	Weidmuller	1594540000.0	1	P1
SMA	Johnson Components	142-0701-851	4	OSCin, OSCin*, RFout, Vcc
TCXO - 100 MHz	Connor-Winfield	CWX813 - 100 MHz	1	Y1
NFET	Fairchild	BSS138	1	U5
VCXO - 100 MHz	CRYSTEK	CVPD-920 – 100 MHz	1	U4
LMX2541	National Semiconductor	LMX2541SQxxxx	1	U1
Standoffs	SPC Technology	SPCS-6	4	Place in Holes at the corners of the board.
		C	pen	
Open	-	Open Capacitor	14	C1_LF, C2pLF, C4_LF, C22, C23, C29, C44, C45, C46, C47
Open		Open Capacitor	6	C100, C101, C102, C103, C104, C105
Open	-	Open Resistor	22	R2pLF,R4_LF, R9, R11, R13, R15, R16, R17, R18, R19, R20, R22, R23, R24, R25, R26, R27, R28, R40, R43, R44, R45
Open	-	Open Resistor	9	R100, R101, R102, R103, R104, R105, R106, R107, R108, R109
Open	-	Open Crystal	1	Y100
Open	-	Open IC	3	U2, U3, U100
Open	-	Open SMA	3	ExtVCOin, Ftest/LD, VccAux



Bottom Assembly Diagram



No Components are assembled on the bottom layer in the default setup.

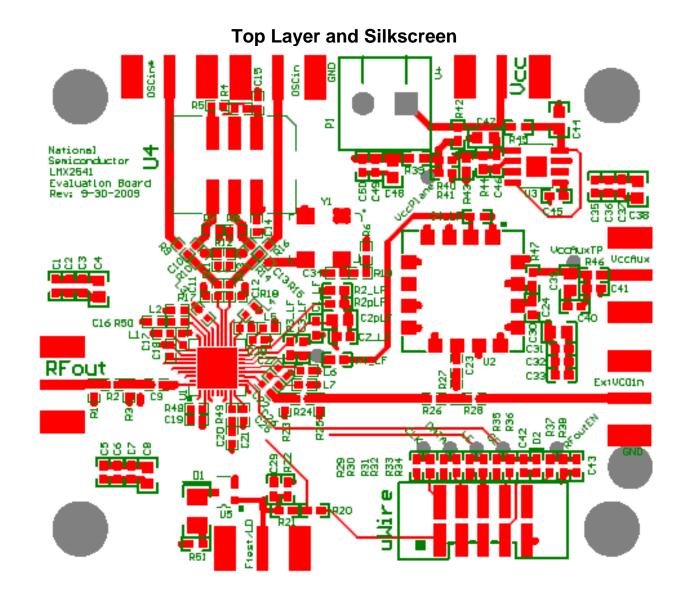


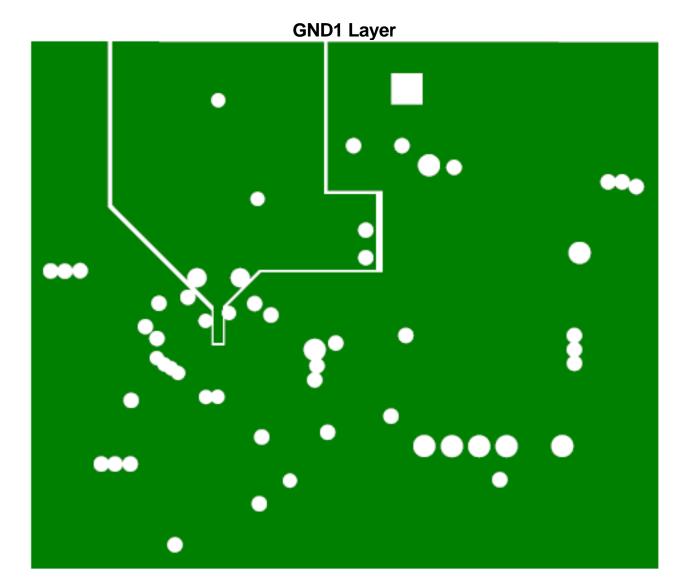
Board Layer Stackup

Board Material	Rogers RO4003
Number of Layers	6
Board Thickness	0.062"
Copper Weight	1 oz Finished
Finish	Immersion Gold
Solder Mask Color	Green/Gloss
Tacting	100% Electrical
Testing	Testing

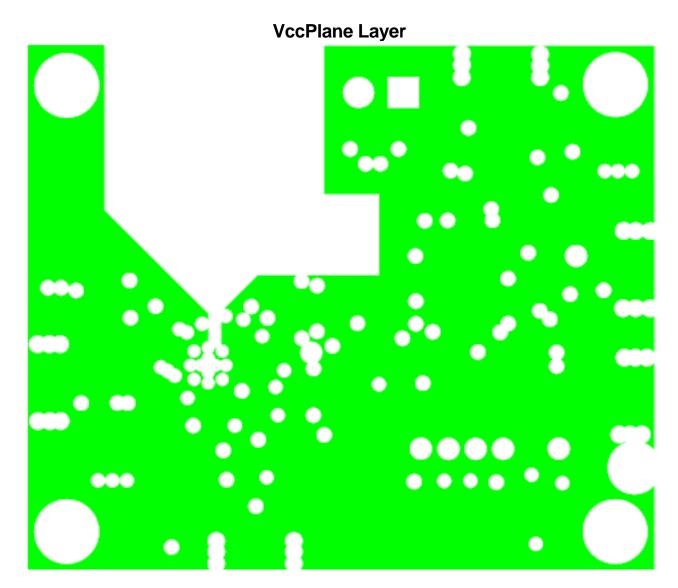
Top Layer 1oz thick	
RO4003 (ϵ_r = 3.38, Tand = 0.0022) CONTROLLED THICKNESS of 16 mils thick	62 1
GND1 Layer	mils tl
FR4 ($\varepsilon_r = \sim 4.6$) ?? mils thick, but thinner is preferable	62 mils thick total
VccPlane Layer	al
FR4 ?? mils thick	
Mid Layer 1	
FR4 ($\varepsilon_r = \sim 4.6$) ?? mils thick, but thinner is preferable	
GND2 Layer	
FR4 ($\varepsilon_r = ~4.6$) = ~4.6) ?? mils thick	
Bottom Layer	 <u> </u>

35



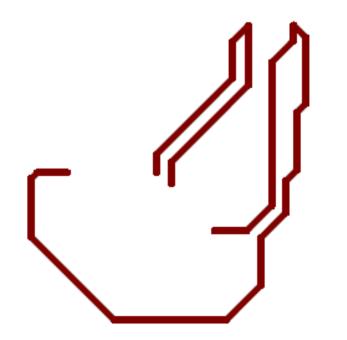


Beneath the TCXO, the ground plane is separated. It is believed that this may improve spurs, especially at offset frequencies equal to the TCXO frequency. These planes are connected on the bottom layer by a small trace.

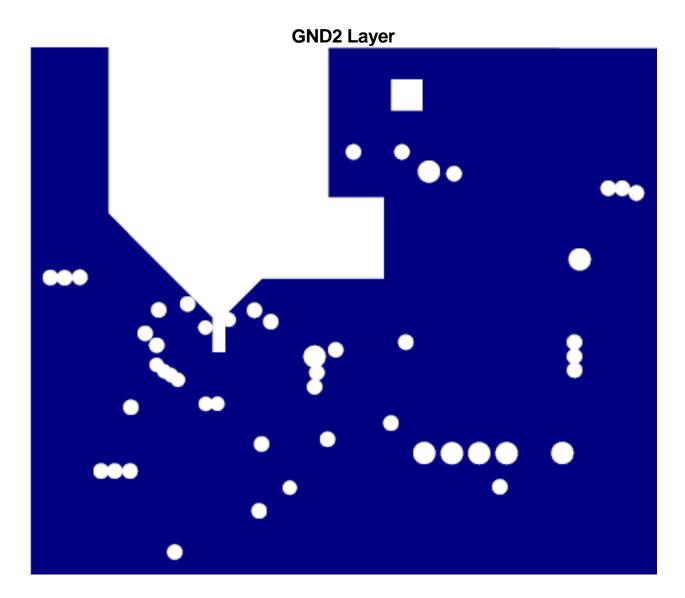


Beneath the TCXO, the power plane is removed to minimize the chance of any noise getting onto this plane.

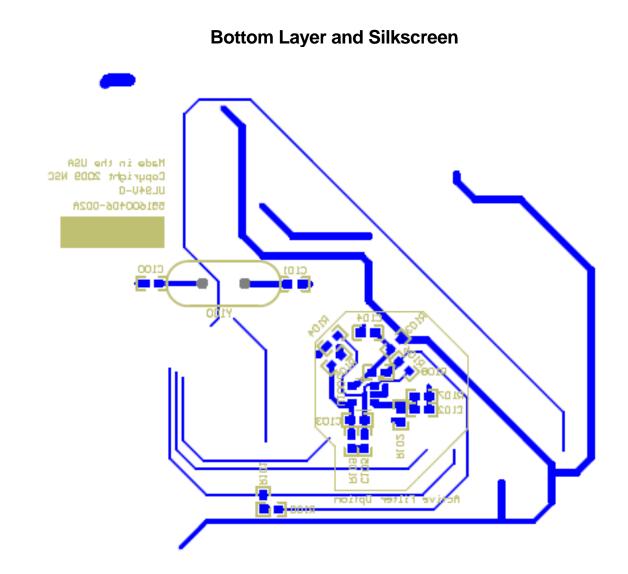
MidLayer 1



Certain pins like VccFRAC and the TCXO supply pins could potentially be sources of noise. These traces were put on this separate layer to try to isolate them more from the



Beneath the TCXO, the ground plane is separated. It is believed that this may improve spurs, especially at offset frequencies equal to the TCXO frequency. These planes are connected on the bottom layer by a small trace.



This layer has the small trace that connects the grounded pieces in the GND1 layer. It has options for an active filter and crystal as well.

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Interface	interface.ti.com	Medical	www.ti.com/medical
Logic	logic.ti.com	Security	www.ti.com/security
Power Mgmt	power.ti.com	Space, Avionics and Defense	www.ti.com/space-avionics-defense
Microcontrollers	microcontroller.ti.com	Video and Imaging	www.ti.com/video
RFID	www.ti-rfid.com		
OMAP Mobile Processors	www.ti.com/omap		
Wireless Connectivity	www.ti.com/wirelessconnectivity		
	TI 505 0		

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