## AN3014 Application note

19 V, 90 W resonant converter with synchronous rectification using the L6563H, L6599A and SRK2000

## Introduction

This application note describes the characteristics and the features of a 90 W demonstration board (EVL90WADP-LLCSR), tailored to specifications for a typical high-end portable computer power supply. A peculiarity of this SMPS design is the very high efficiency compliant with ENERGY STAR ${ }^{\circledR}$ eligibility criteria (EPA rev. 2.0 EPS). One of the key factors in achieving this result is the SRK2000. This synchronous rectification driver for LLC resonant converters allows significantly reduced secondary-side losses. Thanks to this improvement, secondary-side heatsinks, which are typically needed for this power range, can be dramatically reduced or even removed.

Figure 1. EVL90WADP-LLCSR: 90 W adapter demonstration board


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## 1 Main characteristics and circuit description

The main features of the SMPS are

- Universal input mains range: $90-264 \mathrm{Vac}$, frequency $45-65 \mathrm{~Hz}$
- Output voltage: 19 V at 4.75 A continuous operation
- Mains harmonics: according to EN61000-3-2 class-D or JEITA-MITI class-D
- Standby mains consumption: < 0.26 W at 230 Vac
- Efficiency at nominal load: $>92 \%$ at 115 Vac
- EMI: according to EN55022-class-B
- Safety: according to EN60950
- Dimensions: $65 \times 155 \mathrm{~mm}, 25 \mathrm{~mm}$ maximum component height
- PCB: double-sided, $70 \mu \mathrm{~m}$, FR-4, mixed PTH/SMT

The circuit is composed of two stages: a front-end PFC using the L6563H, and a LLC resonant converter based on the L6599A. The SRK2000 controls the synchronous rectification on the secondary side. The PFC stage works as a preregulator and powers the resonant stage with a constant voltage of 400 V . The downstream converter operates only if the PFC is on and regulating. In this way, the resonant stage can be optimized for a narrow input voltage range.

## Startup sequence

As indicated previously, the PFC acts as master and the resonant stage can operate only if the PFC output is delivering the nominal output voltage. Therefore the circuit is designed so that at startup the PFC starts first, then the downstream converter turns on. Initially, the L6563H is supplied by the integrated high voltage startup circuit, but as soon as the PFC starts switching, a charge pump connected to the PFC inductor supplies both the PFC and resonant controllers. Once both stages have been activated, the controllers are supplied also by the auxiliary winding of the resonant transformer, assuring correct supply voltage even during standby operation.

Because the L6563H integrated HV startup circuit is turned off and therefore is not dissipative during normal operation, it significantly contributes to the reduction of power consumption when the power supply operates at light load, in accordance with current world-wide standby consumption standards.

## Brownout protection

Brownout protection prevents the circuit from working with abnormal mains levels. It is easily achieved using the RUN pin (pin12) of the L6563H. This pin is connected through a resistor divider to the VFF pin (pin5), which provides the mains voltage peak value information. An internal comparator enables the IC operations if the mains level is correct, within the nominal limits. At startup, if the input voltage is below 90 Vac (typ), circuit operations are inhibited.

The L6599A has similar protection on the LINE pin (pin 7). It is used to prevent the resonant converter from working with too low an input voltage, which can cause incorrect capacitive mode operation. If the bulk voltage (PFC output) is below 380 V , the resonant startup is not allowed. The L6599A internal comparator has a hysteresis which allows the turn-on and turn-off voltage to be set independently. The turn-off threshold has been set to 300 V in
order to avoid capacitive mode operation, but to allow the resonant stage to operate even in case of mains sag and consequent PFC output dip.

## Fast voltage feed-forward

The voltage on the L6563H VFF pin (pin 5) is the peak value of the voltage on the MULT pin (pin 3). The RC network (R15+R26, C12) connected to VFF completes the peak-holding circuit. This signal is necessary to derive RMS input voltage information to compensate the loop gain, which is mains voltage dependent.

Generally speaking, if the time constant is too small, the voltage generated is affected by a considerable amount of ripple at twice the mains frequency, thus causing distortion of the current reference (resulting in high THD and poor PF). If the time constant is too large, there is a considerable delay in setting the right amount of feed-forward, resulting in excessive overshoot or undershoot of the preregulator's output voltage in response to large line voltage changes.

To overcome this issue, the L6563H implements the new fast voltage feed-forward function. As soon as the voltage on the VFF pin decreases to a set threshold ( 40 mV typically), a mains dip is assumed and an internal switch rapidly discharges the VFF capacitor via a 10$\mathrm{k} \Omega$ resistor. Thanks to this feature, it is possible to set an $R C$ circuit with a long time constant, assuring a low THD and maintaining a fast response to mains dip.

## Resonant power stage

The downstream converter employs ST's L6599A, which incorporates all the functions necessary to properly control the resonant converter with a $50 \%$ fixed duty cycle and works with a variable frequency.

The transformer uses the integrated magnetic approach, incorporating a resonant series inductor. Thus, no additional external coil is needed for the resonance. The transformer configuration chosen for the secondary winding is center tap.

On the secondary side, the output rectification is controlled by the SRK2000, an SR driver dedicated to LLC resonant topology.

A small LC filter has been added on the output, filtering the high-frequency ripple.
D15, R56, R62, R65, R66, Q5 and Q6 implement an output voltage "fast discharge" circuit which quickly discharges the output capacitors when the converter is turned off. It has been implemented to quickly decrease the residual output voltage after the converter is turned off at no load.

## Output voltage feedback loop

The feedback loop is implemented by means of a typical circuit using a TL431 to modulate the current in the optocoupler diode.

On the primary side, R34 - connecting the RFMIN pin (pin 4) to the optocoupler phototransistor - closes the feedback loop and its value sets the maximum switching frequency at about 130 kHz . This value has been chosen to limit the switching losses at light load operation. R31, which connects the same pin to ground, sets the minimum switching frequency. The R-C series (R44 and C18) sets both the soft-start maximum frequency and duration.

## L6599A overload and short-circuit protection

The current into the primary winding is sensed by the lossless circuit R41, C27, D11, D10, R39, and C25 and is fed to the ISEN pin (pin 6). In case of overcurrent, the voltage on the pin passes an internal threshold ( 0.8 V ), triggering a protection sequence. The capacitor (C45) connected to the DELAY pin (pin 2 ) is charged by an internal $150-\mu \mathrm{A}$ current generator and is slowly discharged by the external resistor (R24). If the voltage on the pin reaches 2 V , the soft-start capacitor is completely discharged so that the switching frequency is pushed to its maximum value. As the voltage on the pin exceeds 3.5 V , the IC stops switching and the internal generator is turned off, so that the voltage on the pin decays due to the external resistor. The IC is soft-restarted as the voltage drops below 0.3 V . In this way, under short-circuit conditions, the converter works intermittently with very low input average power.

## Overvoltage and open loop protection

Both the PFC and resonant circuit stages are equipped with their own overvoltage protection.

The PFC controller L6563H monitors its output voltage via the resistor divider connected to a dedicated pin (PFC_OK, pin 7), protecting the circuit in case of loop failures, disconnection or deviation from the nominal value of the feedback loop divider. If the voltage on pin \#7 exceeds 2.5 V the IC stops switching and restarts as the voltage on the pin falls below 2.4 V , preventing the output voltage becoming excessive in case of transient due to the slow response of the error amplifier. However, if contemporaneously the voltage of the INV pin falls below 1.66 V (typ.), a feedback failure is assumed. In this case the PFC_OK circuitry latches the L6563H operations and, by means of the PWM_LATCH pin (pin 8) it latches the L6599A as well, via the DIS pin (pin 8). The converter is kept latched by the L6563H HV circuit which supplies the IC, charging the $\mathrm{V}_{\mathrm{CC}}$ capacitor periodically. To resume converter operation, mains restart is necessary.

The DIS pin is used to protect also the resonant stage against overvoltage. The Zener diode D8 detects the auxiliary voltage, which is proportional to the output voltage. In case of loop failure it conducts and voltage on the DIS pin exceeds the internal threshold, and latches off the device. L6563H operation is also stopped by the PFC_STOP pin.

## Secondary-side synchronous rectification with the SRK2000

The SRK2000 core function is to switch on each synchronous rectifier MOSFET whenever the corresponding transformer half-winding starts conducting (i.e. when the MOSFET body diode starts conducting), and then to switch it off when the current flowing through it approaches zero. For this purpose, the IC is equipped with two pins (DVS1 and DVS2) capable of sensing the MOSFET drain voltage level.

## Standby power saving

The board has a burst-mode function implemented, allowing power saving during light load operation.

The L6599A STBY pin (pin 5) senses the optocoupler's collector voltage, which is related to the feedback control. This signal is compared to an internal reference ( 1.24 V ). If the voltage on the pin is lower than the reference, the IC enters an idle state and its quiescent current is reduced. As the voltage exceeds the reference by 50 mV , the controller restarts the switching. The burst-mode operation load threshold can be programmed by properly choosing the resistor connecting the optocoupler to the RFMIN pin (R34). On this board, the controller operates in burst-mode if the load falls below $\sim 10 \mathrm{~W}$.

The L6563H implements its own burst-mode function. If the COMP voltage falls below 2.5 V , the IC stops switching, causing an output voltage drop. As a consequence, the COMP voltage rise again and the IC starts switching again.

In order to achieve better load transient response, the PFC burst-mode operation is partially forced by the resonant converter: as soon as the L6599A stops switching due to load drops, its PFC_STOP pin pulls down the L6563H's PFC_OK pin, disabling PFC switching. Thanks to this simple circuit, the PFC is forced into an idle state when the resonant stage is not switching, and rapidly wakes up when the downstream converter restarts switching. This solution prevents significant drop of the bulk voltage in case of abrupt load rising.

Figure 2. Electrical diagram


## 2 Efficiency measurement

## EPA rev. $\mathbf{2 . 0}$ external power supply compliance verification

Table 1 shows the no-load consumption and overall efficiency, measured at the nominal mains voltages. At 115 Vac the average efficiency is $91.27 \%$, while at 230 Vac it is $92.22 \%$. Both values are much higher than the $87 \%$ required by the EPA rev 2.0 external power supply limits.

Even at no-load, the board performances are superior: maximum no-load consumption at nominal mains voltage is 260 mW only. This value is significantly lower than the limit imposed by the ENERGY STAR ${ }^{\circledR}$ program, which is 500 mW .

Table 1. Overall efficiency

| Test | $230 \mathrm{~V}-50 \mathrm{~Hz}$ |  |  |  |  | $115 \mathrm{~V}-60 \mathrm{~Hz}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Vout [V] | $\begin{aligned} & \text { lout } \\ & {[\mathrm{mA}]} \end{aligned}$ | Pout <br> [W] | Pin <br> [W] | Eff. <br> [\%] | Vout [V] | $\begin{aligned} & \text { lout } \\ & {[\mathrm{mA}]} \end{aligned}$ | Pout <br> [W] | Pin <br> [W] | Eff. <br> [\%] |
| No load | 18.98 | 0.00 | 0.00 | 0.26 | - | 18.98 | 0.00 | 0.00 | 0.23 | - |
| 25\% load eff. | 18.97 | 1187 | 22.52 | 25.46 | 88.45\% | 18.97 | 1187 | 22.51 | 25.41 | 88.57\% |
| 50\% load eff. | 18.95 | 2375 | 45.01 | 48.70 | 92.42\% | 18.95 | 2374 | 44.99 | 49.03 | 91.77\% |
| 75\% load eff. | 18.94 | 3565 | 67.52 | 71.96 | 93.82\% | 18.94 | 3565 | 67.50 | 73.06 | 92.38\% |
| 100\% load eff. | 18.92 | 4756 | 89.99 | 95.54 | 94.19\% | 18.92 | 4758 | 90.02 | 97.48 | 92.34\% |
| Average eff. |  |  |  |  | 92.22\% |  |  |  |  | 91.27\% |

## Efficiency comparison between diode rectification and synchronous rectification

In Table 2, the efficiency of two different designs are compared. One is the EVL90WADPLLCSR board, and the other is an identical board but with diode rectification (two STPS10L60 devices). In this way, a direct indication of the efficiency improvement obtained with the new synchronous rectification solution is obtained.

Table 2. Efficiency comparison

| Test | 230 V-50 Hz |  |  | 115 V-60 Hz |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Eff. with <br> diodes | Eff. with <br> SRK2000 | Variation | Eff. with <br> diodes | Eff. with <br> SRK2000 | Variation |
| 25\% load eff. | $87.49 \%$ | $88.45 \%$ | $0.96 \%$ | $88.24 \%$ | $88.57 \%$ | $0.33 \%$ |
| $50 \%$ load eff. | $91.52 \%$ | $92.42 \%$ | $0.90 \%$ | $90.85 \%$ | $91.77 \%$ | $0.91 \%$ |
| $75 \%$ load eff. | $92.58 \%$ | $93.82 \%$ | $1.24 \%$ | $91.16 \%$ | $92.38 \%$ | $1.23 \%$ |
| 100\% load eff. | $92.84 \%$ | $94.19 \%$ | $1.35 \%$ | $91.00 \%$ | $92.34 \%$ | $1.34 \%$ |
| Average eff. | $91.11 \%$ | $92.22 \%$ | $1.11 \%$ | $90.31 \%$ | $91.27 \%$ | $0.95 \%$ |

## Light load operation efficiency

Measurement results are reported in Table 3 below and plotted in Figure 3. As shown, efficiency is better than $68 \%$ even for very light loads, such as 1 W .

Table 3. Light load efficiency

| Test | $230 \mathrm{~V}-50 \mathrm{~Hz}$ |  |  |  |  | $115 \mathrm{~V}-60 \mathrm{~Hz}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Vout <br> [V] | $\begin{aligned} & \text { lout } \\ & {[\mathrm{mA}]} \end{aligned}$ | Pout <br> [W] | Pin <br> [W] | Eff. <br> [\%] | Vout [V] | $\begin{aligned} & \text { lout } \\ & {[\mathrm{mA}]} \end{aligned}$ | Pout <br> [W] | Pin <br> [W] | Eff. <br> [\%] |
| 0.25 W | 18.97 | 13.2 | 0.250 | 0.610 | 41.05\% | 18.97 | 13.2 | 0.250 | 0.590 | 42.45\% |
| 0.5 W | 18.97 | 26.4 | 0.501 | 0.877 | 57.18\% | 18.97 | 26.4 | 0.501 | 0.870 | 57.57\% |
| 1.0 W | 18.97 | 52.7 | 0.999 | 1.467 | 68.13\% | 18.97 | 52.7 | 0.999 | 1.457 | 68.60\% |
| 1.5 W | 18.98 | 79.0 | 1.499 | 2.160 | 69.41\% | 18.97 | 79.2 | 1.503 | 2.134 | 70.41\% |
| 2.0 W | 18.97 | 105.5 | 2.002 | 2.822 | 70.93\% | 18.97 | 105.5 | 2.002 | 2.895 | 69.15\% |
| 2.5 W | 18.97 | 131.8 | 2.500 | 3.558 | 70.27\% | 18.98 | 131.8 | 2.501 | 3.711 | 67.38\% |
| 3.0 W | 18.98 | 158.3 | 3.004 | 4.110 | 73.09\% | 18.97 | 158.3 | 3.002 | 4.230 | 70.97\% |
| 3.5 W | 18.97 | 184.5 | 3.501 | 4.660 | 75.13\% | 18.97 | 184.5 | 3.501 | 4.637 | 75.49\% |
| 4.0 W | 18.97 | 210.8 | 3.999 | 5.256 | 76.08\% | 18.97 | 210.8 | 3.999 | 5.234 | 76.40\% |
| 4.5 W | 18.97 | 237.3 | 4.502 | 5.840 | 77.08\% | 18.97 | 237.3 | 4.502 | 5.830 | 77.22\% |
| 5.0 W | 18.97 | 263.6 | 5.000 | 6.450 | 77.52\% | 18.97 | 263.6 | 5.001 | 6.420 | 77.89\% |

Figure 3. Light load efficiency diagram


## 3 Harmonic content measurement

The board has been tested according to the European standard EN61000-3-2 class-D and Japanese standard JEITA-MITI Class-D, at both nominal input voltage mains. As reported in graphs that follow, the circuit is capable of reducing the harmonics well below the limits of both regulations.

Figure 4. Compliance to EN61000-3-2 at 230 Vac - 50 Hz, full load


Figure 5. Compliance to JEITA-MITI at $100 \mathrm{Vac}-50 \mathrm{~Hz}$, full load


At the bottom of the diagrams, the total harmonic distortion and power factor measurements are also reported. The values in all conditions provide a clear overview of the correct functionality of the PFC.

## 4 Functional check

Figure 6 and Figure 7 are waveforms relevant to the resonant stage during steady state operation. The selected switching frequency is approximately 100 kHz in order to achieve a good trade-off between transformer losses and dimensions. The converter operates above the resonance frequency. Figure 7 shows the resonant ZVS operation. Both MOSFETs are turned on when resonant current is flowing through their body diodes and the drain-source voltage is zero.

Figure 6. Resonant stage oscillator at 230 V - 50 Hz - full load


Figure 7. Resonant stage waveforms at 230 V - 50 Hz - full load


In Figure 8, typical waveforms relevant to the secondary side are shown. It can be noted that the rectifier MOSFETs are switched on and off according to the current flowing through them. Figure 9 shows the waveforms during startup at 90 Vac and full load. Here, the sequence of the two stages can be noted: at power-on the L6563H and L6599A V ${ }_{C C}$ voltages increase up to the turn-on thresholds of the two ICs. The PFC starts and its output voltage increases from the mains rectified voltage to its nominal value. In the meantime, the L6599A is kept inactive by the LINE pin (pin 7) until the PFC voltage reaches the set threshold. Then the resonant starts operating and the output voltage reaches the nominal level.

Figure 8. Secondary waveforms at 230 V - 50 Hz

Figure 9. Startup sequencing at 230 V-50 Hz


## Standby and no-load operation

In Figure 10 and Figure 11, some burst-mode waveforms are displayed. As illustrated, both the L6599A and L6563H operate in burst-mode. In Figure 11 it can be observed that the PFC and LLC bursts are synchronized.

Figure 10. No load operation at 230 V-50 Hz


Figure 11. No load operation-detail at 230 V - 50 Hz


In Figure 12 and Figure 13 the transitions from full load to no load and vice-versa at maximum input voltage have been checked. The maximum input voltage has been chosen because it is the most critical input voltage for transition; in fact, at no load the burst pulses have the lower repetition frequency and the $\mathrm{V}_{\mathrm{CC}}$ could drop, causing restart cycles of the controller. As visible in the images, both transitions are clean and there is no output voltage or $\mathrm{V}_{\mathrm{CC}}$ dip.

Figure 12. Transition full load to no load at $265 \mathrm{Vac}-50 \mathrm{~Hz}$


Figure 13. Transition no load to full load at 265 Vac - 50 Hz

## Overcurrent and short-circuit protection

The L6599A is equipped with a current sensing input (pin 6, ISEN) and a dedicated overcurrent management system. The current flowing in the resonant tank is detected and the signal is fed to the ISEN pin. It is internally connected to a first comparator, referenced to 0.8 V , and to a second comparator referenced to 1.5 V . If the voltage externally applied to the pin exceeds 0.8 V , the first comparator is tripped, causing an internal switch to be turned on and discharging the soft-start capacitor CSS.

Under output short-circuit, this operation results in a nearly constant peak primary current.
With the L6599A, designers can externally program the maximum time that the converter is allowed to run in overload or short-circuit conditions. Overloads or short-circuits lasting less than the set time do not cause any protective action, thus providing the system with immunity to short-duration phenomena. If, instead, an overload condition continues, a protection procedure is activated that shuts down the L6599A and, in case of continuous overload/short-circuit, results in continuous intermittent operation with a user-defined duty cycle. This function is realized with the DELAY pin (pin 2) by means of a capacitor (C45) and the parallel resistor R24 connected to ground. If the voltage on the ISEN pin exceeds 0.8 V , the first OCP comparator, in addition to discharging CSS, turns on an internal $150 \mu \mathrm{~A}$ current generator which, via the DELAY pin, charges C45. If the voltage on C45 is 3.5 V , the L6599A stops switching and the PFC_STOP pin is pulled low. Also, the internal generator is turned off, so that C45 is now slowly discharged by R24. The IC restarts when the voltage on C45 is less than 0.3 V . Additionally, if the voltage on the ISEN pin reaches 1.5 V for any reason (e.g. transformer saturation), the second comparator is triggered, the L6599A shuts down, and operation resumes after an off-on cycle.

Figure 14. Short-circuit at full load and 115 Vac - 60 Hz


Figure 15. Short-circuit detail at full load and $115 \mathrm{Vac} \mathbf{- 6 0 ~ H z}$


In the graphs above it can be noted that the average output current as well as the average primary current are limited, preventing converter over-heating and consequent failure.

## 5 Thermal map

In order to check design reliability, thermal mapping by means of an IR camera was done. Below, thermal measurements of the component side of the board at nominal input voltage are shown. The pointers on the images have been placed across key components. The ambient temperature during both measurements was $27^{\circ} \mathrm{C}$.

Figure 16. Thermal map at $115 \mathrm{Vac}-60 \mathrm{~Hz}$ - full load


Figure 17. Thermal map at $230 \mathrm{Vac}-50 \mathrm{~Hz}$ - full load


Table 4. Thermal map reference points

| Point | Reference | Description |
| :---: | :---: | :---: |
| A | L1 | EMI filtering inductor |
| B | D1 | Bridge rectifier |
| C | L2 | PFC inductor |
| D | D4 | PFC output diode |
| E | Q3 | Resonant high-side MOSFET |
| F | Q1 | Resonant power transformer |
| G | Output rectifier MOSFETs (hottest spot) |  |

The pictures highlight that although both the synchronous rectifier MOSFETs at secondary side are working without a heatsink, their operating case temperature is lower than $60^{\circ} \mathrm{C}$.

## 6 Conducted emission pre-compliance test

The following figures represent the average measurement of the conducted noise at full load and nominal mains voltages. The limits shown on the diagrams are those of the EN55022 class-B standard, which is most popular standard for domestic equipment, and sets more severe limits compared to class-A, dedicated to IT technology equipment. As visible in the diagrams, under all test conditions the measurements are well below the limits.

Figure 18. CE average measurement at 115 Vac and full load


Figure 19. CE average measurement at 230 Vac and full load


## 7 Bill of material

Table 5. EVL90WADP-LLCSR demonstration board bill of material

| Des. | Part type/part value | Description | Supplier | Case |
| :---: | :---: | :---: | :---: | :---: |
| C1 | 470 nF | X2 - FLM cap - R46-I 3470--M1- | ARCOTRONICS | $9 \times 18 \mathrm{~mm} \mathrm{P15} \mathrm{~mm}$ |
| C2 | 2.2 nF | Y1 safety cap. DE1E3KX222M | Murata | DWG |
| C3 | 2.2 nF | Y1 safety cap. DE1E3KX222M | Murata | DWG |
| C4 | 470 nF | X2 - FLM cap - R46-I 3470--M1- | ARCOTRONICS | $9 \times 18 \mathrm{~mm} \mathrm{P15} \mathrm{~mm}$ |
| C5 | 470 nF | 400 V - FILM cap - B32653A4474 | EPCOS | DWG |
| C6 | 4.7 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C7 | 100 nF | 100 V CERCAP - general purpose | AVX | PTH |
| C8 | $10 \mu \mathrm{~F}$ | Aluminum ELCAP - YXF series | Rubycon | Dia. $6.3 \times 11 \mathrm{~mm}$ |
| C9 | $47 \mu \mathrm{~F}$ | 450 V aluminum ELCAP - ED series | Panasonic | Dia. $18 \times 32 \mathrm{~mm}$ |
| C10 | 1 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C11 | 2.2 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C12 | $1 \mu \mathrm{~F}$ | 25 V CERCAP - general purpose | AVX | 0805 |
| C13 | 680 nF | 25 V CERCAP - general purpose | AVX | 1206 |
| C14 | 68 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C15 | $47 \mu \mathrm{~F}$ | 50 V aluminum ELCAP - YXF series | Rubycon | Dia. $6.3 \times 11 \mathrm{~mm}$ |
| C16 | 2.2 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C17 | 470 pF | $50 \mathrm{~V}-5 \%$ - COG - CERCAP | AVX | 0805 |
| C18 | $2.2 \mu \mathrm{~F}$ | 6.3 V CERCAP - general purpose | AVX | 1206 |
| C19 | 100 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C20 | 2.2 nF | Y1 safety cap. DE1E3KX222M | Murata | DWG |
| C21 | 2.2 nF | Y1 safety cap. DE1E3KX222M | Murata | DWG |
| C22 | 220 pF | 50 V CERCAP - general purpose | AVX | 0805 |
| C23 | 10 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C24 | $100 \mu \mathrm{~F}$ | 50 V aluminum ELCAP-YXF series | Rubycon | Dia. $10 \times 12.5 \mathrm{~mm}$ |
| C25 | 330 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C26 | $10 \mu \mathrm{~F}$ | 50 V aluminum ELCAP - YXF series | Rubycon | Dia. $6.3 \times 11 \mathrm{~mm}$ |
| C27 | 220 pF | 500 V CERCAP - 5MQ221KAAAA | AVX | $5 \times 3 \mathrm{~mm}$ |
| C28 | 22 nF | 630 V - PHE450MA5220JR05 | KEMET | $16 \times 8 \mathrm{~mm}$ |
| C29 | $470 \mu \mathrm{~F}$ | 35 V aluminum ELCAP - YXF series | Rubycon | Dia. $12.5 \times 20 \mathrm{~mm}$ |
| C30 | $470 \mu \mathrm{~F}$ | 35 V aluminum ELCAP - YXF series | Rubycon | Dia. $12.5 \times 20 \mathrm{~mm}$ |
| C31 | $220 \mu \mathrm{~F}$ | 35 V aluminum ELCAP - FM series | Panasonic | D8x16 |
| C32 | 100 nF | 50 V CERCAP - general purpose | AVX | 0805 |

Table 5. EVL90WADP-LLCSR demonstration board bill of material (continued)

| Des. | Part type/part value | Description | Supplier | Case |
| :---: | :---: | :---: | :---: | :---: |
| C34 | 220 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C36 | $1 \mu \mathrm{~F}$ | 50 V aluminum ELCAP - YXF series | Rubycon | Dia. $6.3 \times 11 \mathrm{~mm}$ |
| C39 | 100 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C40 | 100 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C41 | 100 nF | 50 V CERCAP - general purpose | AVX | 0805 |
| C42 | 100 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C43 | 4.7 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C44 | 10 nF | 50 V CERCAP - general purpose | AVX | 1206 |
| C45 | 220 nF | 25 V CERCAP - general purpose | AVX | 0805 |
| C48 | $10 \mu \mathrm{~F}$ | 50 V aluminum ELCAP - YXF series | Rubycon | Dia. $6.3 \times 11 \mathrm{~mm}$ |
| D1 | GBU4J | Single-phase bridge rectifier | Vishay | GBU |
| D2 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D3 | 1N4005 | General purpose rectifier | Vishay | DO-41 |
| D4 | STTH2L06 | Ultrafast high-voltage rectifier | STMicroelectronics | DO-41 |
| D5 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D7 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D8 | BZV55-B27 | Zener diode | Vishay | SOD-80 |
| D9 | STPS1L60A | Power Schottky rectifier | STMicroelectronics | SMA |
| D10 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D11 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D15 | BZV55-C15 | Zener diode | Vishay | SOD-80 |
| D16 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D18 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D19 | LL4148 | High-speed signal diode | Vishay | SOD-80 |
| D20 | BZV55-B15 | Zener diode | Vishay | SOD-80 |
| D22 | LL4148 | Fast switching diode | Vishay | SOD-80 |
| F1 | Fuse T4A | Fuse 4 A - time lag - 3921400 | Littelfuse | P 5.08 mm |
| HS1 | Heatsink | Heatsink for D1, Q1, Q3, Q4 |  | DWG |
| J1 | MKDS 1,5/3-5,08 | PCB term. block, screw conn., - 3 wires | Phoenix Contact | P 5.08 mm |
| J2 | MKDS 1,5/ 2-5,08 | PCB term. block, screw conn., - 2 wires | Phoenix Contact | P 5.08 mm |
| L1 | HF2826-123Y1R8-T01 | Input EMI filter | TDK | DWG |
| L2 | 1974.0002 | PFC inductor - 0.52 mH | Magnetica | DWG |
| L3 | 1073.0083 | $1 \mu \mathrm{H}-5 \mathrm{~A}$ inductor | Magnetica | DWG |
| Q1 | STF12NM50N | N-channel power MOSFET | STMicroelectronics | TO-220FP |
| Q3 | STP8NM50FP | N-channel power MOSFET | STMicroelectronics | TO-220FP |

Table 5. EVL90WADP-LLCSR demonstration board bill of material (continued)

| Des. | Part type/part value | Description | Supplier | Case |
| :---: | :---: | :---: | :---: | :---: |
| Q4 | STP8NM50FP | N-channel power MOSFET | STMicroelectronics | TO-220FP |
| Q5 | BC847C | NPN small signal BJT | Vishay | SOT-23 |
| Q6 | BC847C | NPN small signal BJT | Vishay | SOT-23 |
| Q9 | BC847C | NPN small signal BJT | Vishay | SOT-23 |
| Q11 | STF60N55F3 | N-channel power MOSFET | STMicroelectronics | TO-220FP |
| Q12 | STF60N55F3 | N-channel power MOSFET | STMicroelectronics | TO-220FP |
| R1 | $3.3 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R2 | $3.3 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R3 | $1 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R4 | 2.2 M | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R5 | $10 \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R6 | NTC 2R5-S237 | NTC resistor P/N B57237S0259M000 | EPCOS | DWG |
| R7 | $1 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R8 | $1 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R9 | $62 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R10 | $27 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R11 | $2.2 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R12 | $2.2 \mathrm{M} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R13 | $10 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R14 | $51 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R15 | $56 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R16 | $4.7 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R17 | $2.2 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R18 | $82 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R19 | $56 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R21 | $39 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R22 | $0.47 \Omega$ | Axial film res -0.4 W-5\%-250 ppm/ ${ }^{\circ} \mathrm{C}$ | Vishay | PTH |
| R23 | $0.82 \Omega$ | Axial film res - $0.4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | PTH |
| R24 | $1 \mathrm{M} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R25 | $56 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R26 | $1 \mathrm{M} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R27 | $470 \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R28 | $33 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R29 | $1.0 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R30 | $10 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |

Table 5. EVL90WADP-LLCSR demonstration board bill of material (continued)

| Des. | Part type/part value | Description | Supplier | Case |
| :---: | :---: | :---: | :---: | :---: |
| R31 | $15 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R32 | $47 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R34 | $3.3 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R35 | $180 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R37 | $220 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R38 | $56 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R39 | $130 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R40 | $0.0 \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R41 | $100 \Omega$ | Axial film res-0.4 W-5\%-250 ppm/ ${ }^{\circ} \mathrm{C}$ | Vishay | PTH |
| R42 | $4.7 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R43 | $51 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R44 | $4.3 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R46 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R47 | $1.0 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R48 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R49 | $39 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R50 | $6.2 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R51 | $120 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-1 \%-100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R53 | $0.0 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R54 | $0.0 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R56 | $18 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R58 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R59 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R60 | $10 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R62 | $4.7 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R63 | $27 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R64 | $27 \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R65 | $47 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R66 | $2.2 \mathrm{k} \Omega$ | SMD film res - $1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| R68 | $7.5 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R69 | $4.7 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R74 | $3.9 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R75 | $3.9 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R76 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R77 | $100 \mathrm{k} \Omega$ | SMD film res - $1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |

Table 5. EVL90WADP-LLCSR demonstration board bill of material (continued)

| Des. | Part type/part value | Description | Supplier | Case |
| :---: | :---: | :---: | :---: | :---: |
| R78 | $33 \mathrm{k} \Omega$ | SMD film res $-1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R79 | $150 \mathrm{k} \Omega$ | SMD film res $-1 / 8 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 0805 |
| R80 | $0.0 \Omega$ | SMD film res $-1 / 4 \mathrm{~W}-5 \%-250 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | Vishay | 1206 |
| T1 | 1860.0025 | Resonant power transformer | Magnetica | DWG |
| U1 | L6563H | High voltage startup TM PFC controller | STMicroelectronics | SO-16 |
| U3 | SFH617A-2 | Optocoupler | Infineon | DIP-4 |
| U4 | TL431AIZ | Programmable shunt voltage reference | STMicroelectronics | TO-92 |
| U5 | SRK2000 | Synch. rect. driver for LLC res conv | STMicroelectronics | SO-8 |
| U6 | L6599A | Improved HV resonant controller | STMicroelectronics | SO-16 |

## 8 PFC coil specification

## General description and characteristics

- Application type: consumer, home appliance
- Transformer type: open
- Coil former: vertical type, 6+6 pins
- Max. temperature rise: $45^{\circ} \mathrm{C}$
- Max. operating ambient temperature: $60^{\circ} \mathrm{C}$
- Mains insulation: N.A.
- Unit finishing: varnished


## Electrical characteristics

- Converter topology: boost, transition mode
- Core type: PQ26/20-PC44 or equivalent
- Min. operating frequency: 40 kHz
- Typical operating frequency: 120 kHz
- Primary inductance: $520 \mu \mathrm{H} \pm 10 \%$ at $1 \mathrm{kHz}-0.25 \mathrm{~V}$ (see note below)
- Peak primary current: 4.2 Apk

Note: $\quad$ Measured between pins 5 and 9.

## Electrical diagram and winding characteristics

Figure 20. PFC coil electrical


Table 6. PFC coil winding data

| Pins | Windings | RMS current | Number of turns | Wire type |
| :---: | :---: | :---: | :---: | :---: |
| $11-3$ | AUX | $0.05 \mathrm{~A}_{\mathrm{RMS}}$ | 5.5 | $\phi 0.28 \mathrm{~mm}-\mathrm{G} 2$ |
| $5-9$ | Primary | $1.4 \mathrm{~A}_{\mathrm{RMS}}$ | 57.5 | $30 \times \phi 0.1 \mathrm{~mm}-\mathrm{G} 1$ |

## Mechanical aspect and pin numbering

- Maximum height from PCB: 22 mm
- Coil former type: vertical, 6+6 pins (pins 1, 2, 4, 6, 7, 10, 12 are removed)
- Pin distance: 3.81 mm
- Row distance: 25 mm
- External copper shield: not insulated, wound around the ferrite core and including the coil former. Height is 8 mm . Connected to pin 3 by a soldered solid wire.

Figure 21. PFC coil mechanical aspect


## Manufacturer

- Magnetica - Italy
- Inductor P/N: 1974.0002


## 9 Transformer specification

## General description and characteristics

- Application type: consumer, home appliance
- Transformer type: open
- Coil former: horizontal type, 7+7 pins, two slots
- Max. temperature rise: $45^{\circ} \mathrm{C}$
- Max. operating ambient temperature: $60^{\circ} \mathrm{C}$
- Mains insulation: in accordance with EN60950


## Electrical characteristics

- Converter topology: half bridge, resonant
- Core type: ETD34-PC44 or equivalent
- Min. operating frequency: 60 kHz
- Typical operating frequency: 100 kHz
- Primary inductance: $1200 \mu \mathrm{H} \pm 10 \%$ at $1 \mathrm{kHz}-0.25 \mathrm{~V}$ (see Note 1)
- Leakage inductance: $200 \mu \mathrm{H} \pm 10 \%$ at $100 \mathrm{kHz}-0.25 \mathrm{~V}$ (see Note 2)

Note: 1 Measured between pins 2-4
2 Measured between pins 2-4 with only one secondary winding shorted

## Electrical diagram and winding characteristics

Figure 22. Transformer electrical diagram


Table 7. Transformer winding data

| Pins | Winding | RMS current | Number of turns | Wire type |
| :---: | :---: | :---: | :---: | :---: |
| $2-4$ | Primary | $1 A_{\text {RMS }}$ | 50 | $30 \times \phi 0.1 \mathrm{~mm}-\mathrm{G} 1$ |
| $14-13$ | Sec - A | $(1)$ | $4 A_{\text {RMS }}$ | 5 |
| $12-11$ | Sec - $B^{(1)}$ | $4 A_{\text {RMS }}$ | 5 | $90 \times \phi 0.1 \mathrm{~mm}-\mathrm{G} 1$ |
| $5-6$ | Aux $^{(2)}$ | $0.05 \mathrm{~A}_{\text {RMS }}$ | $4 \mathrm{~mm}-\mathrm{G} 1$ |  |

[^0]2. Aux winding is wound on top of primary winding

## Mechanical aspect and pin numbering

- Maximum height from PCB: 30 mm
- Coil former type: horizontal, 7+7 pins (pins 1 and 7 are removed)
- Pin distance: 5.08 mm
- Row distance: 25.4 mm

Figure 23. Transformer overall drawing


## Manufacturer

- Magnetica - Italy
- Transformer P/N: 1860.0025


## 10 Revision history

Table 8. Document revision history

| Date | Revision | Changes |
| :---: | :---: | :--- |
| 22-Mar-2010 | 1 | Initial release. |
| 13-Dec-2010 | 2 | Updated Chapter 1 |

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[^0]:    1. Secondary windings $A$ and $B$ are in parallel
